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## HA12181FP

AM Radio Noise Reduction System

## Renesns

ADE-207-171A (Z)
2nd. Edition
June 1997

## Functions

- Buffer amp. for audio
- Linear approximate circuit for noise reduction
- IF Amp., detector, audio amp. and AGC circuit for noise detection
- Gate pulse generator


## Features

- High noise cancelling capacity: 46 dB typ.
- Less gain loss: $\mathrm{G}_{\mathrm{v}}=-0.5 \mathrm{~dB}$ typ.
- Low total harmonic destortion and high signal-to noise ratio: THD $=0.06 \%$ typ., $\mathrm{S} / \mathrm{N}=75 \mathrm{~dB}$ typ.
- Operation supply voltage range: 7.0 V to $10 \mathrm{~V}(8.2 \mathrm{~V}$ typ.)
- Less external parts count


## HA12181FP

## Block Diagram



## Table of Pin Description and External Parts



## HA12181FP

Table of Pin Description and External Parts (cont)

| No. of pin | Name | Function | DC voltage (V) (No input) | Equivalent circuit | External parts |  | Influence of External parts |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | No. | recom- <br> mended <br> value | Larger than recommended value | Smaller than recommended value |
| 6 | Hold | Hold of level difference. | 3.3 | 6 $=\begin{aligned} & C 511 \\ & = \\ & \\ & 0.033 \mu\end{aligned}$ | C511 | $0.033 \mu$ | Must be recomme | d on the ed value. |
| 7 | GND | GND |  | - | - | - | - | - |
| 8 | High- <br> Pass. | High- <br> Pass <br> AMP. <br> (Wave- <br> form <br> Compensation) | 3.3 | 8 $=\begin{aligned} & C 510 \\ & = \\ & \\ & 0.033 \mu\end{aligned}$ | C510 | $0.033 \mu$ | Must be recomme | ed on the ded value. |
| 9 | AF out | Output of |  |  | C508 | $1 \mu$ | Output |  |
|  |  | AF |  |  | R504 | 4.7 K | Output load |  |
| 10 | Wave form | Waveform Compensation | 3.3 |  | C509 | $0.033 \mu$ | Must be recomme | d on the ed value. |

Table of Pin Description and External Parts (cont)

| No. of pin | Name | Function | DC voltage (V) (No input) | Equivalent circuit | External parts |  | Influence of External parts |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | No. | recom- <br> mended <br> value | Larger than recommended value | Smaller than recommended value |
| 11 | Gate | Gate |  |  | R503 | 180 K |  |  |
|  |  | pulse generation | $\prod_{0}^{4.5 \mathrm{~V}} \square$ |  | C507 | 2200 P | pulse width become wider. | pulse width become narrow. |
| 12 | Vth | Determination of noise detection sensitivit y | $1.1$ |  | R502 | 22 K | Higher noise detection sensitivity. | Lower noise detection sensitivity. |
| 13 | $\mathrm{V}_{\mathrm{cc}}$ | $\mathrm{V}_{\mathrm{cc}}$ | 8.2 | - | - | - | - | - |
| 14 | IF Det. | IF AGC detector | 3.3 |  | C503 | $0.01 \mu$ | - | - |
| 15 | AF | Time | 0 |  | R505 | 47 K | Longer | Miss- |
|  | AGC | constant <br> for AF <br> AGC |  |  | C504 | $0.22 \mu$ | time to stabilize AGC. | operaton in noise detector. |

## HA12181FP

Table of Pin Description and External Parts (cont)


Absolute Maximum Ratings $\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$

| Item | Symbol | Rating | Unit |
| :--- | :--- | :--- | :--- |
| Supply voltage | $\mathrm{V}_{\mathrm{cc}}$ | 16 | V |
| Power dissipation | Pd | $400^{\star 1}$ | mW |
| Operating temperature | Topr | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature | Tstg | -55 to +125 | ${ }^{\circ} \mathrm{C}$ |

Note: 1. Value at $\mathrm{Ta}=85^{\circ} \mathrm{C}$

Electrical Characteristics (Tentative) $\left(\mathrm{V}_{\mathrm{CC}}=8.2 \mathrm{~V}, \mathrm{Ta}=25^{\circ} \mathrm{C}\right.$, Pin 3 input: Vin $=100$ $\mathrm{mVrms}, \mathrm{f}=1 \mathrm{KHz}$, Pin 16 input: Vin $=74 \mathrm{~dB} \mu$, $\mathrm{fc}=450 \mathrm{KHz}, \mathrm{fm}=1 \mathrm{KHz}, \mathrm{m}=30 \%$ )

| Item | Symbol | Min | Typ | Max | Unit | Test conditions |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Supply current | $\mathrm{I}_{\mathrm{cc}}$ | - | 11.0 | - | mA | No input signal, IC only |
| Output voltage | Vout | 70 | 95 | 120 | mVrms | Pin 3 input only |
| Total harmonic distortion | THD 1 | - | 0.06 | 0.3 | $\%$ |  |
| Signal-to-noise ratio | $\mathrm{S} / \mathrm{N}(1)$ | 60 | 75 | - | dB | Pin 3 input Vin $=100 \mathrm{mVrms}$ <br> (Reference), $\mathrm{Rg}=10 \mathrm{~K} \Omega$ |
| Strong input total harmonic <br> distortion | THD 2 | - | 1.0 | 2.5 | $\%$ | Pin 3 input Vin $=500 \mathrm{mVrms}$ |
| Recovered output voltage | $\mathrm{V}_{\mathrm{o}}(\mathrm{AF})$ | 50 | 78 | 120 | mVrms | Pin 16 input only |
| Recovered output signal-to- <br> noise-ratio | $\mathrm{S} / \mathrm{N}(2)$ | 35 | 45 | - | dB |  |
| Noise suppression ratio | NSR | 35 | 46 | - | dB | Input the waveform below. <br> Pin 3 input Vin $=100 \mathrm{mVrms}$ <br> (Reference) no input sine wave |



Figure 1 Input Waveform at Measurement of Noise Suppression Ratio

## HA12181FP

## Test Circuit



## Operation Principle



Figure 2 System Block Diagram of AM Radio

A system block diagram of AM Radio using the HA12181FP is shown in Figure 2 and waveforms at each point in the system are illustrated in Figure 3. For AM wave with impulse noise from ANT, the pulse spreads its width each time when the AM wave passes through a selection filter.

The pulse width becomes the order of several hundred microseconds at detector output (Point C).
A radio without a noise canceller produces large noise to the audience. This IC perfectly detects every noise by using the signals from 1st IFT (Point B) in front of the narrow band filter.

The wave process circuit approximates the voltage linearly at the pulse to reduce the noise in the output.
The principle for wave processing follows. Further investigation make it clear that the pulse width of impulse noise is constant (several handred microseconds) and independent of the waveform or waveheight.

Therefore the former and later voltage (VA, VB) of the pulse can be found at the same time (T1) by means of the wave and the delayed one for this time, as shown in the right figure.


Figure 3 Waveforms at Each Point in the System
In an actual circuit, the differential voltage between input and output of phase shift circuit is changed to the capacitor C511 at pin 6.

At the time of T1, when the switch turns to the noise processing mode (the switch positions in Figure 4 are inverted), the voltage difference (VA - VB) is held in C511.

C509 at pin 10 is changed by the differential voltage between the held voltage and the output voltage at pin $9(\mathrm{VA}): \mathrm{VA}-(\mathrm{VA}-\mathrm{VB})=\mathrm{VB}$.

## HA12181FP

As the initial voltage of C509 is equal to the output voltage (VA) before the switch change, the voltage between terminals of C509 is changed from VA to VB.

The waveform which change up to C509 becomes the output, because the voltage of C509 appears at pin 9 through the buffer.

The changed up waveform of C509 is almost linearly approximated because of the constant current change by the feedback from the output at pin 9 .

At the time of T 2 when the awitches change to the normal mode (the switch position in Figure 4), the output recovers smoothly as the voltage of C509 is VB.

However the unmatch of the wave delay time due to the pulse width or the phase circuit and the offset of circuit make a slight step difference on the waverform at the moment of switch change.

LPF, consisting of R1 and C509 make it smooth.
The frequency characteristics, which is detriorated by LPF in the normalmode, is compensated so that it might become flat. C509 and C510 should have the same capacity, and the tolerance must be within $\pm 5 \%$.


Figure 4 Waveform Processing Circuit

## Evaluation Circuit for Noise Reduction Effect



## HA12181FP

## Example of Noise Reduction Effect




## PC Board Layout Pattern


(Top view)

(Bottom view)

## HA12181FP

## Main Characteristics







## HA12181FP




## HA12181FP

## Package Dimensions



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